PRESSURE FILTRATION IN A CRACKED AND POROUS STRATUM

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The main assumptions of the theory for nonsteady-state filtration in a cracked and porous material are given in [1]. A general solution is given in the present work for the first and second boundary problems of filtration in cracks.

1. We assume that pressure equals zero in a cracked and porous material occupying a half-space $x \ge 0$. From instant t = 0 at boundary x = 0 pressure starts to change by the rule $p_1(t, 0) = f(t)$. The distribution of pressure in cracks is determined from solution of the problem in [1]

$$\frac{\partial p_1}{\partial t} = \varkappa \frac{\partial^2 p_1}{\partial x^2} + \eta \frac{\partial^3 p_1}{\partial x^2 \partial t}; \tag{1.1}$$

$$p_1(t,0) = f(t); (1.2)$$

$$\varkappa \frac{\partial^2 p_1(0,x)}{\partial x^2} - A p_1(0,x) = -A p_2(0,x);$$

$$p_2(0,x) = 0, \ p_1(0,0) = f(0).$$
(1.3)

Here p_1 , p_2 are the pressures in cracks and blocks; \varkappa , η , A are coefficients introduced in [1] where it was shown that the initial pressure distribution in cracks should be found from problem (1.3) whose solution is

$$p_1(0,x) = f(0)\exp(-x/\sqrt{\eta}).$$
 (1.4)

It is easy to prove; the solution of the first boundary problem (1.1), (1.2), (1.4) is a function

$$p_{1}(t,x) = \frac{2\kappa}{\pi} \int_{0}^{t} f(u) \int_{0}^{\infty} \exp(-\kappa(t-u)\beta^{2}/(1+\eta\beta^{2})) \frac{\beta \sin(x\beta)}{(1+\eta\beta^{2})^{2}} d\beta du + f(t)\exp(-\kappa/\sqrt{\eta}).$$
(1.5)

With $\eta \rightarrow 0$ problem (1.1), (1.2), (1.4) is converted into the first boundary problem for the piezoelectric conductivity equation [2, Eq. (861.21)]

$$\frac{\partial p_1}{\partial t} = \varkappa \frac{\partial^2 p_1}{\partial x^2}, \ p_1(t,0) = f(t), \ p_1(0,x) = 0, \tag{1.6}$$

and its solution is converted into the solution of problem (1.6)

$$\lim_{\eta \to 0} \left[\frac{2\varkappa}{\pi} \int_{0}^{t} f(u) \int_{0}^{\infty} \exp(-\varkappa(t-u)\beta^{2}/(1+\eta\beta^{2})) \frac{\beta \sin(x\beta)}{(1+\eta\beta^{2})^{2}} d\beta du + f(t) \exp(-\varkappa/\sqrt{\eta}) \right] = \frac{2\varkappa}{\pi} \int_{0}^{t} f(u) \int_{0}^{\infty} \exp(-\varkappa(t-u)\beta^{2})\beta \sin(x\beta) d\beta du = \frac{x}{2\sqrt{\pi\varkappa}} \int_{0}^{t} f(u)(t-u)^{-3/2} \exp(-\varkappa^{2}/4\varkappa(t-u)) du.$$

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It is noted that the pressure in blocks is determined from the equation in [1]

$$p_2(t,x) = p_1(t,x) - \frac{\varkappa}{A} \frac{\partial^2 p_1(t,x)}{\partial x^2}.$$

2. We consider the problem of flow towards a drainage gallery. Then conditions (1.2), (1.4), and solution (1.5) are written in the form

$$p_{1}(t,0) = p_{0} = \text{const}, \ p_{1}(0,x) = p_{0}\exp(-x/\sqrt{\eta}),$$

$$p_{1}(t,x) = p_{0}\left[1 - \frac{2}{\pi}\int_{0}^{\infty}\exp\left(-\frac{2\pi}{\eta}\frac{\beta^{2}}{1+\beta^{2}}\right)\frac{\sin\left((x/\sqrt{\eta})\beta\right)}{\beta(1+\beta^{2})}d\beta\right].$$
(2.1)

We calculate the flow of liquid through boundary x = 0. By differentiating expression (2.1) with respect to x with x = 0 we obtain

$$q = -\frac{k_1}{\mu} \frac{\partial \rho_1}{\partial x} \Big|_{x=0} = \frac{2\rho_0 k_1}{\pi \sqrt{\eta} \mu} \int_0^\infty \exp\left(-\frac{\varkappa d}{\eta} \frac{\beta^2}{1+\beta^2}\right) \frac{d\beta}{1+\beta^2},$$
 (2.2)

where k_1 is crack permeability; μ is liquid viscosity. By using the Laplace method (see for example [3]) we find asymptotic expressions for pressure (2.1) with small x and flow (2.2) with $t \rightarrow \infty$:

$$p_1(t,x) \sim p_0 \left(1 - \frac{x}{\sqrt{\pi \varkappa t}} \left(1 + \frac{\eta}{4\varkappa t}\right)\right), \ q \sim \frac{p_0}{\sqrt{\pi \varkappa t}} \left(1 + \frac{\eta}{4\varkappa t}\right).$$
(2.3)

It can be seen from expression (2.3) that with filtration in porous material ($\eta = 0$) the pressure will be greater and the flow will be less than with a cracked and porous material. This is connected with the fact that as a result of exchange of liquid between blocks and cracks liquid entering a boundary is partly released by blocks adjacent to it. It is found that blocks are 'run-offs' for pressure from cracks and 'sources' of liquid for cracks. With $t < \eta/x$ from relationship (2.2) we obtain

$$q(t) \sim \frac{p_0 k_1}{\sqrt{\eta} \mu} \left(1 - \frac{1}{2} \frac{\kappa t}{\eta} \right).$$
 (2.4)

3. We find pressure distribution with prescribed flow of liquid through a boundary (second boundary problem). For this we replace boundary condition (1.2) as flows:

$$\frac{\partial \rho_1(t,0)}{\partial x} = -\frac{\mu}{k_1} q(t). \tag{3.1}$$

Correspondingly initial condition (1.4) is also changed:

$$p_1(0,x) = \frac{\mu}{k_1} q(0) \sqrt{\eta} \exp(-x/\sqrt{\eta}).$$
(3.2)

It is easy to prove that the solution of the problem (1.1), (3.1), (3.2) is given by the equation

$$p_{1}(t,x) = \frac{2\varkappa\mu}{\pi k_{1}} \int_{0}^{t} q(u) \int_{0}^{\infty} \exp\left(-\varkappa(t-u)\frac{\beta^{2}}{1+\eta\beta^{2}}\right) \frac{\cos(x\beta)}{(1+\eta\beta^{2})^{2}} d\beta du + \frac{\mu}{k_{1}} q(t)\sqrt{\eta} \exp(-\varkappa/\sqrt{\eta}).$$
(3.3)

with $q(t) = q_0 = \text{const from relationship} (3.3)$ we have

$$p_{1}(t,x) = \frac{\mu}{k_{1}} q_{0} \left[\frac{2}{\pi} \int_{0}^{\infty} \frac{1 - \exp(-\varkappa d\beta^{2}/(1 + \eta\beta^{2}))}{\beta^{2}} \frac{\cos(\varkappa \beta)}{1 + \eta\beta^{2}} d\beta + \sqrt{\eta} \exp(-\varkappa/\sqrt{\eta}) \right].$$
(3.4)

With t < η/x it follows from relationship (3.4) that

$$p_1(t,0) \sim \frac{\mu}{k_1} q_0 \sqrt{\eta} \left(1 + \frac{1}{2} \frac{\varkappa t}{\eta}\right).$$
 (3.5)

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It can be seen by comparing Eqs. (2.4) and (3.5) that they are similar to each other since the latter may be converted

$$q_0 \sim \frac{p_1(t,0)k_1}{\sqrt{\eta}\mu} \frac{1}{1 + \frac{1}{2}\frac{\kappa_1}{\eta}} \sim \frac{p_1(t,0)k_1}{\sqrt{\eta}\mu} \left(1 - \frac{1}{2}\frac{\kappa_1}{\eta}\right),$$

and from them it follows that in order to maintain a constant flow of liquid through the boundary pressure should increase linearly, but with a fixed pressure in the gallery flow decreases linearly.

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